



A Decade-Bandwidth Distributed Power Amplifier MMIC Using 0.25 μm GaN HEMT Technology

Dong-Hwan Shin^{1,2} · In-Bok Yom¹ · Dong-Wook Kim^{2,*}

Abstract

This study presents a 2–20 GHz monolithic distributed power amplifier (DPA) using a 0.25 μm AlGaIn/GaN on SiC high electron mobility transistor (HEMT) technology. The gate width of the HEMT was selected after considering the input capacitance of the unit cell that guarantees decade bandwidth. To achieve high output power using small transistors, a 12-stage DPA was designed with a non-uniform drain line impedance to provide optimal output power matching. The maximum operating frequency of the proposed DPA is above 20 GHz, which is higher than those of other DPAs manufactured with the same gate-length process. The measured output power and power-added efficiency of the DPA monolithic microwave integrated circuit (MMIC) are 35.3–38.6 dBm and 11.4%–31%, respectively, for 2–20 GHz.

Key Words: Decade Bandwidth, Distributed Power Amplifier, High Power Amplifier, MMIC, 0.25 μm AlGaIn/GaN HEMT.

I. INTRODUCTION

Recently developed microwave systems require increasingly wider operating bandwidth. Especially electronic warfare systems are required to operate in multi-octave bandwidth. An ultra-wideband power amplifier is one of the most challenging components to be implemented in electronic warfare systems. Currently, such ultra-wideband power amplifier can be implemented with AlGaIn/GaN high electron mobility transistor (HEMT) monolithic microwave integrated circuit (MMIC) technology, which has rapidly developed over the past several years [1].

Compared to other amplifier structures that use lossy matching or balanced topologies, a distributed amplifier (DA) is advantageous for wideband operations because in the DA configuration gate-source capacitance and drain-source capacitance of

each transistor are absorbed into the artificial transmission line structure. The bandwidth of the DA is determined by the dominant low-pass cutoff frequency of input or output artificial transmission lines [2]. Therefore, the smaller capacitance of the transistor results in wider bandwidth in the DA configuration.

This paper presents the design and fabrication of a distributed power amplifier (DPA) MMIC with decade-bandwidth using 0.25 μm GaN HEMT technology. The maximum operating frequency of the proposed DPA is above 20 GHz, which is higher than those of other DPAs manufactured using the same gate-length process.

II. UNIT CELL DESIGN FOR BANDWIDTH ENHANCEMENT

The DPA MMIC fabrication process is GH25-10 of United Monolithic Semiconductors, which provides 0.25 μm AlGaIn

Manuscript received September 7, 2017 ; Revised October 10, 2017 ; Accepted October 12, 2017. (ID No. 20170907-048J)

¹Satellite Technology Research Group, Electronics and Telecommunications Research Institute, Daejeon, Korea.

²Department of Radio Science and Engineering, Chungnam National University, Daejeon, Korea.

*Corresponding Author: Dong-Wook Kim (e-mail: dwkim21c@cnu.ac.kr)

This is an Open-Access article distributed under the terms of the Creative Commons Attribution Non-Commercial License (<http://creativecommons.org/licenses/by-nc/4.0>) which permits unrestricted non-commercial use, distribution, and reproduction in any medium, provided the original work is properly cited.

© Copyright The Korean Institute of Electromagnetic Engineering and Science. All Rights Reserved.

/GaN HEMTs on SiC substrates. The gate capacitance in the input transmission line has a value substantially larger than the drain capacitance in the output transmission line and determines the dominant cutoff frequency of the DPA [2]. For the DPA to have a cutoff frequency of over 20 GHz, the gate capacitance of a constituent unit cell should be less than 0.3 pF. A schematic diagram and an input equivalent circuit of the unit cell are illustrated in Fig. 1. The gate-source capacitance, C_{gs} , and distributed channel resistance, R_i , are input intrinsic elements of GaN HEMT. These intrinsic elements could be extracted through small-signal admittance parameters. The R_S - C_S parallel network is intentionally inserted to extend the cutoff frequency and stabilizes the amplifier.

The gate capacitance of the unit cell can be reduced through insertion of a series-connected coupling capacitor (C_s). However, in a large peripheral HEMT, the C_{gs} tends to increase rapidly with the frequency, which limits the peripheral size of the HEMT that can be used to achieve a multi-octave band DPA. Fig. 2 shows the equivalent capacitance of a unit cell composed of $4 \times 100 \mu\text{m}$ HEMT and C_s of 0.3 pF and a unit cell composed of $4 \times 50 \mu\text{m}$ HEMT and C_s of 0.3 pF. Applying the former to the DPA design is advantageous in obtaining larger output power, but the operating frequency is restricted to less than 16 GHz. Therefore, the latter should be selected in order to obtain a sufficiently high cutoff frequency above 20 GHz.

III. DISTRIBUTED POWER AMPLIFIER DESIGN

A conventional DPA, called as a non-uniform DPA (NDPA), is designed using non-uniform drain lines, non-uniform transistor size or both to improve an output power and a power-added efficiency (PAE) [3, 4]. The schematic circuit diagram of the DPA is shown in Fig. 3. In an NDPA architecture, the device size of the first cell (Q_1) is usually larger than those of the rest unit cells for optimal power matching. However, in this study, we used $4 \times 50 \mu\text{m}$ HEMTs in all unit cells to extend the bandwidth.

The use of small peripheral HEMTs slightly reduces the output power but can increase the number of stages in the DPA because large characteristic impedances are required for optimal power matching in the drain lines. We used 12 stages in the

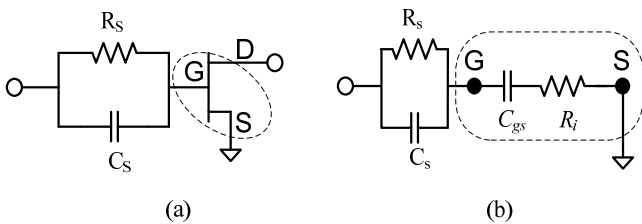


Fig. 1. (a) Schematic diagram of capacitive coupled GaN HEMT and (b) input equivalent circuit at the gate.

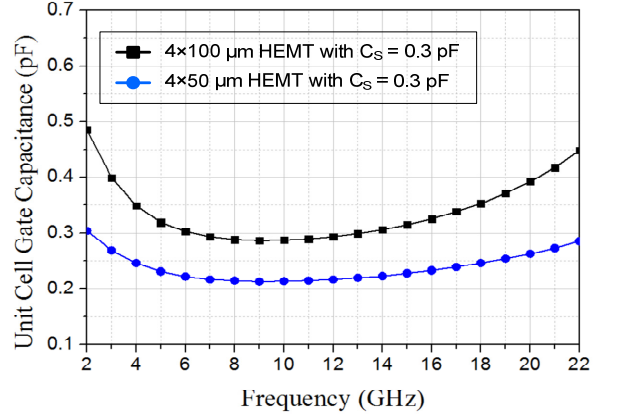


Fig. 2. Equivalent gate capacitance of unit cell with frequency.

DPA to increase the output power within the feasible characteristic impedance range of the drain line. Layout effects including transmission lines, discontinuities and inductors were electromagnetically simulated to include coupling and radiation effects. A photograph of the fabricated decade-bandwidth DPA MMIC is shown in Fig. 4. The chip dimensions are $6.45 \text{ mm} \times 2.35 \text{ mm}$.

IV. MEASURED RESULTS

The fabricated DPA MMIC was mounted on a test jig for the measurement. The test jig consists of a carrier with a power circuit board, two $50\text{-}\Omega$ lines, an aluminum housing and two K-connectors. The DPA MMIC is biased at a drain-source voltage of 28 V and a drain current of 600 mA. The small- and

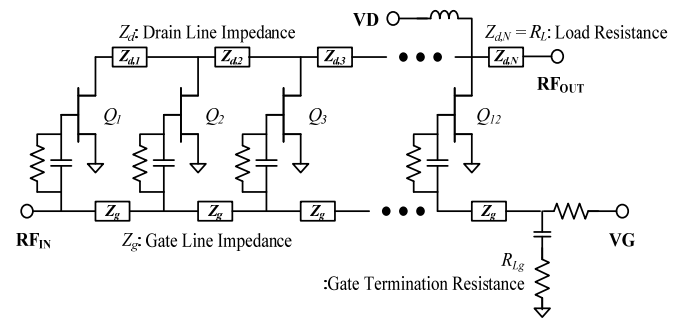


Fig. 3. Schematic diagram of the proposed bandwidth-enhanced DPA.

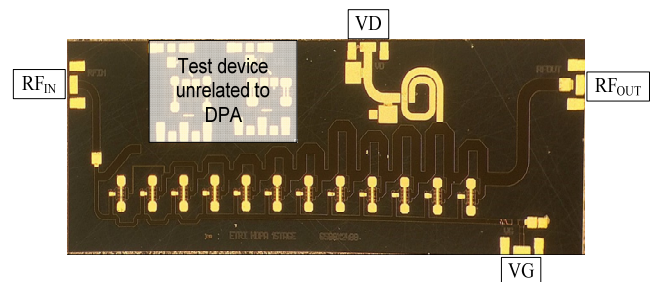


Fig. 4. Photograph of the decade bandwidth DPA MMIC.

large-signal measurements were performed in continuous mode.

Fig. 5 shows the measured and simulated S -parameters of the DPA MMIC. Measured small signal gain is 8.4–11.2 dB, and the input/output return losses are typically 10 dB or more from 2 to 20 GHz. The measured output power and PAE of the DPA MMIC are shown in Fig. 6. In 2–20 GHz, the output power is 35.3–38.6 dBm and the PAE is 11.4%–31%.

The performance of state-of-the-art DPA MMICs fabricated using the 0.25 μm GaN HEMT process is summarized in Table 1. Regarding the operating frequency, this work is competitive with state-of-the-art results.

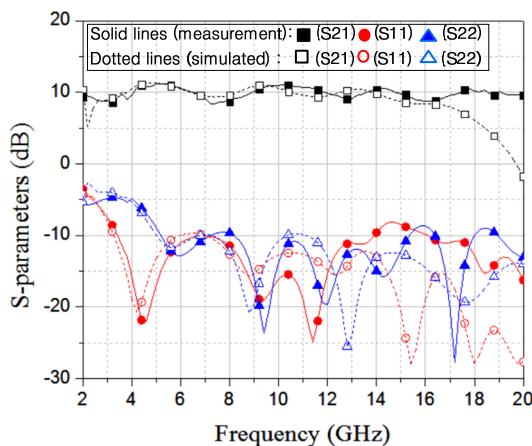


Fig. 5. Measured and simulated S -parameters of the DPA MMIC.

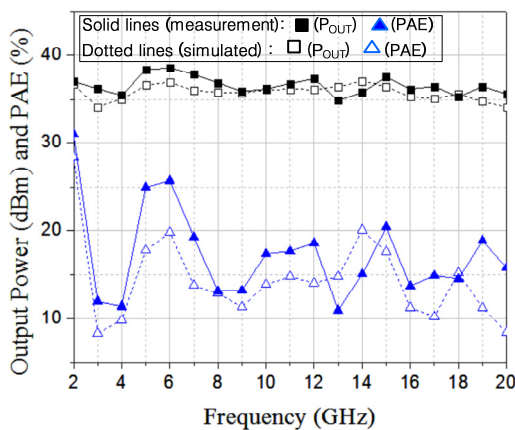


Fig. 6. Measured and simulated output power and PAE of the DPA MMIC.

Table 1. Performance comparison of GaN DPA MMICs fabricated using a 0.25 μm GaN process

Ref.	Freq. (GHz)	P_{OUT} (W)	PAE (%)	Area (mm^2)
[4]	1.5–17	9–15	20–38	15.35
[5]	2–16	4.3–6.9	20–32	10.0
[6]	6–18	6.2–10.2	7.4–16	6.7
[7]	6–16	8–18	7–17	9.19
This work	2–20	3.4–7.2	11.4–31	15.16

V. CONCLUSION

A 2–20 GHz DPA MMIC was demonstrated using a 0.25 μm GaN HEMT process, and the results were presented. The proposed DPA successfully achieved flat gain and output power up to 20 GHz through the design of a unit cell that supported decade bandwidth.

This work was supported by National Research Foundation of Korea (NRF) grant funded by the Korea government (MSIP) (No. NRF-2015M1A3A3A03027459).

REFERENCES

- [1] R. Pengelly, S. Wood, J. Milligan, S. Sheppard, and W. Pribble, "A review of GaN on SiC high electron-mobility power transistors and MMICs," *IEEE Transactions on Microwave Theory and Techniques*, vol. 60, no. 6, pp. 1764–1783, 2012.
- [2] G. Vendelin, A. Pavio, and U. Rohde, *Microwave Circuit Design Using Linear and Nonlinear Techniques*. New York, NY: John Wiley & Sons, 2005.
- [3] C. Duperrier, M. Campovecchio, L. Roussel, M. Lajugie, and R. Quere, "New design method of uniform and non-uniform distributed power amplifiers," *IEEE Transactions on Microwave Theory and Techniques*, vol. 49, no. 12, pp. 2494–2500, 2001.
- [4] C. Campbell, C. Lee, M. Kao, H. Tserng, P. Saunier, and T. Balisteri, "A wideband power amplifier MMIC utilizing GaN on SiC HEMT technology," *IEEE Journal of Solid-State Circuits*, vol. 44, no.10, pp. 2640–2647, 2009.
- [5] J. Gassmann, P. Watson, L. Kehias, and G. Henry, "Wideband, high-efficiency GaN power amplifiers utilizing a non-uniform distributed topology," in *Proceedings of IEEE MTT-S International Microwave Symposium*, Honolulu, HI, 2007, pp. 615–618.
- [6] J. Kim, H. Park, S. Lee, and Y. Kwon, "6–18 GHz, 8.1 W size-efficient GaN distributed amplifier MMIC," *Electronics Letters*, vol. 52, no. 8, pp. 622–624, 2016.
- [7] H. Park, W. Lee, J. Jung, K. Choi, J. Kim, W. Lee, C. Lee, and Y. Kwon, "A 6–16 GHz GaN distributed power amplifier MMIC using self-bias," *Journal of Electromagnetic Engineering and Science*, vol. 17, no. 2, pp. 105–107, 2017.