Toroidal-Shaped Coils for a Wireless Power Transfer System for an Unmanned Aerial Vehicle

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Abstract

Unmanned aerial vehicles (UAVs) using communications, sensors, and navigation equipment will play a key role in future warfare. Currently, UAVs are monitored to prevent misfire and accidents, and the conventional method adopted uses wires for data transmission and power supply. The repeated connection and disconnection of cables increases maintenance time and harms the connector. For convenience and stability, a wireless power transfer system to power UAVs is needed. Unlike other wireless power transfer (WPT) applications, the size of the receiving coils must be small, so that the WPT systems can be embedded inside space-limited UAVs. The small size reduces the coupling coefficient and transfer efficiency between the transmitting and the receiving coils. In this study, we propose a toroidal-shaped coil for a WPT system for UAVs with high coupling coefficient with minimum space requirements. For validation, conventional coils and the proposed toroidal-shaped coil were used and their coupling coefficient and power transfer efficiency were compared using simulated and measured results. The simulated and measured results were strongly correlated, confirming that the proposed WPT system significantly improved efficiency with negligible change in the space requirement.

Key Words: Coupling Coefficient, Power Transfer Efficiency, Unmanned Aerial Vehicles, Wireless Charging, Wireless Power Transfer.

I. INTRODUCTION

Modern and future warfare is shifting toward a space environment with manned and unmanned weapons. The need for unmanned aerial vehicles (UAVs) is increasing. The modern military weapons system is based on the use of communication, sensors, and navigation equipment to accomplish a given task, even in hard-to-reach areas [1]. UAVs include all types of equipment, including drones, satellites, and missiles, among others. However, as UAVs become more advanced, their maintenance and repair also require a higher level of scientific

technology. Conventional UAVs depend on fuel cells with high-energy density for operations. The fuel cell will not stop burning once it has been ignited [2]. UAVs with fuel cells have a 10-year life span. They can avoid misfire and accidents by conducting periodic safety maintenance of the charging and power supply systems. The current UAV power supply maintenance method is shown in Fig. 1 [3]. However, this maintenance method has three problems. First, a large number of direct cables must be connected and then disassembled each time to supply the power. This condition increases the possibility that maintenance time is expanded or that maintenance efficiency is

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Fig. 1. Conventional method for charging and repairing an unmanned vehicle [3].

low. Second, the repeated connection and disconnection of cables causes wear and tear to the connector. It also has the potential to diminish the performance of UAVs. Third, when the UAVs are deployed, the launcher is destroyed every time because the power supply cables and modules are still connected when the UAVs are launched. The demand for wireless power transfer (WPT) technology is increasing because of these and other umbilical cable shortcomings. Therefore, WPT technologies have recently been developed to overcome the limitations of the wired power transfer system [4, 5].

Although WPT technology can overcome the shortcomings of a wired power system, there is concern that the transmission distance poses a potential inconvenience to users [6]. Various coil systems and methods have been employed to increase the transmission distance [7, 8]. However, these enhancing methods generally require increased space, weight, and cost, which are critical problems in UAVs.

In this study, we propose a toroidal-shaped coil for the WPT systems of UAVs. The toroidal-shaped coil includes a wing-shaped ferrite located at the ends of the coil. The toroidal-shaped coil increases the transmission distance by increasing the coupling coefficient between the source and the load coils. It can be applied in UAVs because it requires minimal space, which is an important feature in UAVs.

II. WPT COIL SYSTEMS AS THE CORDLESS UMBILICAL CONNECTOR OF A UAV

To transfer several hundred Watts or more of power with high efficiency in a WPT environment within a few centimeters, a magnetic induction-type WPT technology should be used. The magnetic induction-type WPT system in a UAV typically includes an inverter, a resonance matching capacitor, two magnetically coupled coils, and an AC-DC convertor, as shown in Fig. 2.

Fig. 2. Concept of the wireless power transfer system for unmanned vehicles.

In the WPT system used in this study for a UAV, the air gap from the launch ramp to the UAV is 50 mm, as shown in Fig. 3. The body and the WPT coil case is made of aluminum, similar to the body of the UAV. The skin depth of the aluminum at 110 kHz is 247.25 μm , and the thickness of the aluminum coil case is 3 mm. Therefore, the magnetic field generated by the WPT coil cannot affect the inside of the UAV where the other systems are located.

For miniaturization, the inverter for supplying AC power is located at the bottom of the source coil. The rectifying circuits are directly mounted on the body of the UAV to optimize space.

Conventionally, the size of the transmitting and receiving coils needs to be small because of the limited space in UAVs. However, the small size and the long distance between the transmitting and the receiving coils mean that the coupling coefficient is also small, which can reduce the power transfer effi-

Fig. 3. Configuration of wireless power transfer system for unmanned vehicle.

ciency. At the same transmission distance, a larger-sized WPT Tx coil produces greater power transmission efficiency. Therefore, the coil sizes are chosen according to the given Rx space.

1. Conventional WPT Coil 1 for the Cordless Umbilical Connector of UAVs

A conventional WPT coil 1 [9] is simply a loop coil of the ferromagnetic material with resonance matching capacitance. This WPT coil is simple to design and implement in UAVs, as shown in Fig. 4. Given the small size of the transmitting and receiving coils, the coupling coefficient is small and can cause the diminution of the power transfer efficiency. The geometrical parameters of the conventional WPT coil 1 are shown in Table 1. The material properties of the WPT system for UAVs are presented in Table 2.

When the highly permeable ferrite is designed with a convex shape, its magnetoresistance becomes lower than that of planar ferrite. In the convex configuration, the ferrite acts as a shaped magnetic field in resonance (SMFIR), which forms a magnetic flux generated by the magneto motive force of the coil along the ferrite with a low magnetic reluctance [10]. A schematic illustrating the concept of the magnetic field formed by the SMFIR is shown in Fig. 5. As a result of this design, the magnetic flux generated by the current flowing in the transmitting part is tightly linked to the receiving part.

However, when the size of the coil is much smaller than the distance between the two coils, the coupling coefficient (K) is limited. The size of the conventional coil 1 is shown in Table 1.

The vertical direction of the magnetic flux generated by the source coil (or load coil) is captured by the load coil (or source coil) ferrite. The narrow effective area of the ferrite is shown in Fig. 4. The magnetic flux cannot link the opposite coil, thus

Fig. 4. Over all view of conventional WPT system 1 for UAVs.

Table 1. Geometrical parameters of conventional coil (CC) and proposed toroidal-shaped coil

Parameter	CC 1	CC 2	Proposed coil
Tx coil size (mm)	$70 \times 60 \times 33$	$140 \times 50 \times 20$	$140 \times 50 \times 20$
Rx coil size (mm)	$50 \times 40 \times 22$	$146 \times 40 \times 22$	$50 \times 40 \times 22$
Rx wing size (mm)	-	-	$48 \times 34 \times 3$
Tx turns (turns)	19	19	19
Rx turns (turns)	15	8	8
Air gap (mm)	50	50	50

Table 2. Material properties of WPT systems for UAVs

Parameter	Ferrite	Aluminum	Copper
Conductivity (S/m)	$1.0 \text{ e-}2$	$3.8 \text{ e}7$	$5.8 \text{ e}7$
Relative permeability	1000	1	1

Fig. 5. Schematic of the shaped magnetic field with a conventional coil (b) and the proposed toroidal coil (a) using a ferromagnet.

causing the WPT coil system to have a low coupling coefficient. For higher power transfer efficiency, a broader effective area of ferrite is needed.

2. Conventional WPT Coil 2 for a Cordless Umbilical Connector of UAVs

A conventional WPT coil 2 [9] has a loop coil and a ferromagnetic material with resonance matching capacitance. As shown in Table 1, the conventional WPT system 2 has a larger coil size to increase the coupling coefficient. As the effective area increases, the volume of the coil system also greatly increases (Fig. 6).

The electronic and mechanic devices of UAVs are embedded

Fig. 6. Overall view of the conventional WPT system 2 for UAVs.

Fig. 7. Application of (a) conventional WPT system 1. (b) conventional WPT system 2. (c) proposed toroidal-shaped WPT system.

inside the craft to protect against external impact. Therefore, the coil system should not require an increased volume. Otherwise, it cannot be applied as a UAV WPT system because any increase in the volume of the WPT system limits the load of other devices in the UAV, as shown in Fig. 7(b).

3. Proposed Toroidal-Shaped Coil for Cordless Umbilical Connector of UAVs

The proposed toroidal-shaped coil has a transversely wound coil and a wing-shaped ferrite. The toroidal-shaped coil is wound the same as a solenoidal coil, as shown in Fig. 5. The

Fig. 8. Overall view of the proposed toroidal-shaped WPT coils for UAVs.

size of the proposed toroidal-shaped coil is listed in Table 1. The volume of the transmitting coil is the same as that of the conventional coil system 1.

Unlike its interior, the exterior surface of the UAV can be easily used without spatial limitation. To take advantage of the unused surface area, the wing-shaped ferrite was designed with a thin flat bar shape, as shown in Fig. 8.

The wing-shaped ferrite can minimize the use of the internal space of UAVs and at the same time widen the effective area of the ferrite. The proposed coil can be embedded into the UAV, as shown in Fig. 7(c). The increased area of the proposed coil system is much smaller than that of the conventional coil 2. The proposed coil can increase the coupling coefficient without affecting the volume inside the UAV.

The increased effective area of ferrite can also reduce reluctance. That is, when the WPT coil system has a broader effective area of ferrite, the reluctance of the WPT coil system is reduced. The proposed toroidal coil maximizes the effective area of ferrite, which can increase the coupling coefficient with a minimal increase in space.

III. SIMULATION OF THE WPT SYSTEM FOR A CORDLESS UMBILICAL CONNECTOR OF UAVS

1. Simulation Setup

In the simulation, the operating frequency was set to 110 kHz, and a sinusoidal current flowed through the transmitting coil for a 300-W power transfer. To design the receiving and transmitting coils of the WPT system, a finite element analysis-based magnetic field simulation was used (ANSYS Maxwell Simulation; ANSYS Inc., Canonsburg, PA, USA).

The simulations were conducted under three conditions: a conventional WPT coil 1, a conventional WPT coil 2, and the proposed toroidal-shaped coil. Fig. 9 shows the overall simula-

Fig. 9. Overall setup for the simulation.

tion setup for each coil. The geometrical parameters of each coil system are shown in Table 1. The cross-section of the conventional coils and the proposed toroidal-shaped coil are illustrated in Fig. 10.

Fig. 10. Side view of the simulation configuration. (a) Conventional WPT coil system 1, (b) conventional WPT coil system 2, and (c) proposed toroidal-shaped coil system.

Although the total size of the proposed coil system is slightly larger than that of the conventional coil system 1, the volume inside the UAV is the same, and the increased volume of the coil is applied to the surface of the UAV that is not being used to mount the device.

Three-dimensional (3D) finite element analysis simulations (ANSYS Maxwell) were conducted to compare the electrical parameters of the two structures listed in Table 3. The resistances of the Tx and Rx coils were calculated using a simulation with an ideal environment, where the skin effect and the proximity effect were neglected. To compare the power transfer efficiency, a circuit simulation was performed. The values of the compensation capacitors of the transmitting and receiving coils were determined on the basis of the operating frequency, and a full bridge rectifier and a smoothing capacitor were constructed.

2. Comparison of Power Transfer Efficiencies

The input power of the system is the power supplied from the DC power supply in front of the transmitting coil. The power delivered to the receiver is measured at the back of the receiving coil. The overall system efficiency is the ratio of the power delivered to the load to the system input power. The simulation results are shown in Table 4. The conventional coil system 1 has low power transfer efficiency because of the different sizes of the transmitting and receiving coils. The aluminum

Table 3. Electrical parameters of the conventional coils (CC) and the proposed toroidal-shaped coil

Parameter	CC 1	CC 2	Proposed coil
Tx resistance (mΩ)	5.58	13.25	24.19
Rx resistance (mΩ)	5.51	7.89	11.23
Tx self-inductance (μH)	64.61	181.0	31.15
Tx matching capacitor (nF)	32.39	11.56	67.20
Rx self-inductance (μH)	6.01	2.76	9.90
Rx matching capacitor (nF)	348.20	758.48	211.33
Mutual inductance (μH)	0.28	0.67	3.71
Coupling coefficient	0.014	0.030	0.21
Resonance frequency (kHz)	110	110	110

Table 4. Simulated input, output power, and power transfer efficiency of conventional coils (CC) and the proposed toroidal-shaped coil

Parameter	CC 1	CC 2	Proposed coil
Input power (W)	633.7	467.6	365.7
Output power (W)	299.9	303.1	309.5
Power transfer efficiency (%)	47.3	64.8	84.6

case around the receiving coil decreases the coupling coefficient by canceling the magnetic flux generated by the eddy currents on the aluminum.

The conventional coil system 2 is found to have increased power transfer efficiency in comparison with the conventional coil system 1 because the transmitting and receiving coils were similar in size. The canceling magnetic field from the aluminum case around the receiving coil has lesser effect on the coupling coefficient between the two coils.

The wing ferrite can capture the magnetic flux generated by the opposite coil, thus increasing the coupling coefficient. By using the wing ferrite, the proposed toroidal-shaped coil increased the power transfer efficiency by 37.3%. The wing ferrite, which is included in the proposed toroidal-shaped coil system, has a dramatic effect on the power transfer efficiency of the WPT system, with minimal additional space requirements.

IV. MEASUREMENT OF THE WPT SYSTEM FOR A CORDLESS UMBILICAL CONNECTOR OF UAVS

The power transfer efficiency of the proposed toroidal-shaped coil was measured for comparison with the simulated results. As shown in Fig. 11, a 300-W WPT coil system was designed and implemented to experimentally verify the effectiveness of the proposed toroidal-shaped coil. A Litz wire was used for the coil

Fig. 11. Manufactured toroidal-shaped coil. (a) Transmitting coil and (b) receiving coil.

Fig. 12. Configuration of the WPT system for measurement.

Table 5. Comparison of the simulated and measured input, output power, and power transfer efficiency

Parameter	Simulated	Measured
Input power (W)	365.7	360.3
Output power (W)	309.5	302.7
Power transfer efficiency (%)	84.6	84.0

winding to increase the power transfer efficiency by reducing the resistance of the proposed toroidal-shaped coil.

The resonance frequencies of the transmitting and receiving coils were set to 110 kHz as in the simulations. Consistent with the simulations, the power delivered to the load was 300 W, and the voltage targeted was at 28 V. Therefore, the resistance of the electronic load was set to 2.55 Ω .

The size of the coils and the distance between the source and the receiving coils were the same as those in the simulation environment. The overall coil configuration of the experiment is presented in Fig. 12. The case of the source and receiving coils was made with aluminum, which was also used for the case of the UAV. The air gap consisted of acrylic, which did not affect the generation or linkage of the magnetic field. A full-bridge inverter was used to convert DC power to AC power.

Table 5 shows the input power, output power, and efficiency calculated by measuring the current and the voltage at each point. The measurement data correlated well with the simulation data. The proposed toroidal-shaped coil system dramatically increased the power transfer efficiency.

V. CONCLUSION

In this study, we propose a toroidal-shaped coil system using a wing-shaped ferrite to overcome the reduced efficiency resulting from the small coil size of conventional WPT systems, which is their inherent limit, for UAVs. The design and analysis of the proposed toroidal-shaped coil were performed, and comparisons with other coil systems were conducted using simulations and measurements. The simulation results were in good agreement with the results obtained by measurement.

The simulation and measurement results confirm that the proposed toroidal-shaped coil dramatically increases the power transfer efficiency and is significantly better than the other conventional coil systems in UAVs, with a negligible increase in occupied space.

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