I. INTRODUCTION

The approach of designing an antenna and a photovoltaic cell on the same substrate is useful for reducing costs. However, designing them separately is inefficient for reducing the size and weight of an Internet of Things (IoT) system. Many recent studies have explored the integration of photovoltaic cells with antennas because of the potential advantages of wireless communication. An effective approach is stacking or overlaying to reduce the size and weight. The challenge in this approach is to increase sunlight exposure when the antenna is placed on top of the photovoltaic cell [1–4].

Several techniques, such as the use of a mesh antenna [2, 3] and transparent material [5], have been employed to increase sunlight exposure. Usually, when the antenna and photovoltaic cell are integrated, they are independent of each other [6–12]. In some cases, however, the photovoltaic cell is a part of the antenna and thus enhances the performance of the antenna. An aluminum layer in the solar cell is used as a ground plane for the antenna [13] to provide a reduced footprint, and the solar cell metasurfaces are used to obtain enhanced bandwidth characteristics [14, 15]. Researchers have designed state-of-the-art photovoltaic cell-integrated antennas that are large in size with complex geometries. Given the advances in the application of IoT technologies, simple and compact low-profile photovoltaic built-in antennas that can be easily attached to IoT devices are needed.

In this paper, a compact single-device photovoltaic cell-integrated antenna is proposed for IoT applications. Typically, the antenna and the photovoltaic cell are used separately, thereby occupying substantial real estate. The need for small low-profile devices that can be easily integrated into IoT devices was a consideration. The designed antenna has a low profile and small size; therefore, it can save crucial real estate when used with IoT devices. The designed photovoltaic cell-integrated antenna has 100% sunlight exposure and exhibits excellent an-
tenna characteristics (impedance bandwidth, gain, and radiation pattern). In addition, the photovoltaic cell-integrated slot antenna has an omnidirectional radiation pattern, which is valuable for IoT applications.

II. PHOTOVOLTAIC CELL-INTEGRATED ANTENNA GEOMETRY

Fig. 1 shows the geometry of the photovoltaic cell-integrated slot antenna. A photovoltaic cell made of GaAs was used for integration with the slot antenna. The thickness of the GaAs layer ($\varepsilon_r = 12.9$ and $\tan\delta = 0.0004$) was $h_2 = 0.385$ mm. The photovoltaic cell was configured as follows: a metal grid lined with two bus bars was printed on the top side of the GaAs layer. The grid lines were spaced at a distance of $p = 1.975$ mm apart. The values for the width of the grid line and bus bar were $g_w = 0.1$ mm and $b_s = 1$ mm, respectively. A metallic bottom contact is placed under the GaAs layer. The metallic bottom contact of the photovoltaic cell also served as a ground plane for the slot antenna. For resonance, a slot was cut in the bottom contact of the photovoltaic cell. An alternating current (AC) blocking circuit implemented with a 59 nH inductor was used to prevent the flow of radio frequency (RF) current towards the solar cell. A connecting patch was used to connect one inductor terminal to the antenna ground plane. The other inductor terminal was connected to the bus bar. Fig. 1(a), (c), and (d) show the top, side, and three-dimensional (3D) views, respectively, of the photovoltaic cell-integrated slot antenna. The detailed structure and characteristics of the photovoltaic cells used in this work were presented in [16] and [17].

Fig. 1(b) illustrates the detailed geometry of the slot antenna, which comprises a microstrip feedline, substrate, and ground

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![Diagram](image-url)
plane. A simple slot structure was used so that there would be a minimal effect on the performance of the photovoltaic cell. Moreover, slot antennas are smaller in size, low profile, and they can be easily integrated into planar and/or non-planar surfaces. To design the slot antenna, a Rogers RO4003 substrate with a dielectric constant of $\varepsilon_r = 3.38$ and a loss tangent of $\tan\delta = 0.0027$ was used. The size of the substrate was $L \times W$ and a thickness of 0.508 mm. The metallic bottom contact for the photovoltaic cell, which had a slot size of $L_a \times W_a$, was also used as the ground plane. The dimensions of the slot controlled the resonance frequency of the slot antenna. A 50 $\Omega$ microstrip feedline was placed under the substrate to excite the slot. A quarter-wavelength transformer with a size of $Q_l \times Q_w$ was introduced between the slot and the microstrip feedline to improve impedance matching. The designed photovoltaic cell-integrated slot antenna was simulated with an ANSYS high-frequency structure simulator. The final parameter values for the designed photovoltaic cell-integrated slot antenna are as follows: $h_1 = 0.508$ mm, $h_2 = 0.385$ mm, $W = 25$ mm, $L = 31.75$ mm, $L_1 = 29.5$ mm, $L_2 = 2.25$ mm, $L_a = 12.5$ mm, $W_a = 2.1$ mm, $Q_l = 0.25$ mm, $Q_w = 11.7$ mm, $F_w = 1.3$ mm, $F_l = 4.25$ mm, and $L_m = 0.25$ mm.

### III. Measured and Simulated Results

A prototype of the proposed photovoltaic cell slot-integrated antenna was fabricated and measured to verify the simulation results regarding the reflection coefficient and radiation properties. A photograph of the fabricated prototype is presented in Fig. 2. The reflection coefficient of the fabricated photovoltaic cell slot integrated antenna was measured with a R&S ZVA67 network analyzer (Rohde and Schwarz, Munich, Germany). The measured and simulated reflection coefficients are presented in Fig. 3. The figure indicates that acceptable agreement was found between the simulated and measured reflection coefficients. The measured impedance bandwidth of the fabricated prototype was 270 MHz, from 5.63 GHz to 5.9 GHz, with an increase of 40 MHz as compared to a simulation result that was 230 MHz, from 5.59 GHz to 5.82 GHz.

![Fig. 2. Fabricated prototype.](image)

The measured and simulated reflection coefficients are illustrated in Fig. 3. The maximum simulated gain was 3.41 dBi; however, it fell slightly to a maximum of 3 dBi within the impedance bandwidth. This reduction could be attributed to the measurement setup; thus, it is more likely to have been a measurement error. The designed photovoltaic cell-integrated slot antenna has a dipole-like omnidirectional radiation pattern. Its radiation characteristics did not change in the presence or absence of the photovoltaic cell. The radiation characteristics were measured in a full anechoic chamber at the RFID/USN Center, Incheon, Republic of Korea. The size of the full anechoic chamber was $15.2$ m ($W$) $\times 7.9$ m ($L$) $\times 7.9$ m ($H$). A horn antenna was used as a transmitter, and the fabricated photovoltaic cell antenna was used as a receiver. The transmitter and receiver were separated by a distance of 10 m. The photovoltaic cell antenna was moved circularly from $–180^\circ$ to $180^\circ$ while the horn antenna was fixed. The measured and simulated radiation patterns of the designed photovoltaic cell-integrated slot antenna at 5.70 GHz are shown in Fig. 5. The illustration reveals that the measured and simulated radiation patterns were in relatively good agreement in both the E- and H-planes. The measured results showed that there were some fluctuations in both planes. These fluctuations
could have resulted from using tape and foam rack in the measurement setup. A performance comparison of the proposed photovoltaic cell antenna with other designs is presented in Table 1.

### IV. CONCLUSION

A compact low-profile photovoltaic cell-integrated slot antenna has been presented for IoT applications. The metallic bottom contact of the photovoltaic cell was used as a ground plane for the antenna, and a slot was etched on it for resonance. An AC blocking circuit was used to limit the RF current flow towards the solar cell. Therefore, the proposed photovoltaic cell-integrated slot antenna can function simultaneously as an antenna and a photovoltaic cell. In addition, the antenna exhibited excellent gain performance and a stable omnidirectional radiation pattern within the impedance bandwidth. The low profile, compact size, 100% exposure to light, and good performance of the proposed antenna make it suitable for use as an on-board power source for low-power IoT applications and sensor technologies.

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### REFERENCES


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