Novel CPW-Fed Gamma-Shaped Circularly Polarized Slot Antenna for UWB Applications

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Abstract

In recent years, ultra-wideband (UWB) technology has garnered significant attention for enabling exceptional precision in applications, such as positioning and radar systems. This letter presents a novel coplanar waveguide-fed circularly polarized slot antenna specifically designed for UWB applications. The proposed antenna incorporates innovative elements, including an asymmetric ground equipped with gamma-shaped slits for circular polarization and a gamma-shaped monopole to enhance reflection coefficients. The overall size of the proposed antenna is $18 \text{ mm} \times 18 \text{ mm} \times 1.2 \text{ mm}$ ($0.37\lambda_0 \times 0.37\lambda_0 \times 0.02\lambda_0$). The measurement results demonstrate a reflection coefficient that is consistently below $-10 \text{ dB}$ from 6.10 GHz to 10 GHz, and an axial ratio below 3 dB from 5.70 GHz to 8.50 GHz. Furthermore, the radiation patterns closely match the simulation results. Additionally, this study analyzes antenna and system fidelity factors using time-domain analysis.

Key Words: UWB, Circular Polarization, CPW-Fed Antenna, Time-Domain Analysis.
this work investigates antenna and system fidelity factors to evaluate UWB pulse distortion, which is a critical aspect in the realm of UWB technology [8].

II. DESIGN AND MEASUREMENT

Fig. 1 illustrates the design and fabrication steps involved in creating the proposed antenna, including its final dimensions (unit: mm). All antennas were designed on an 18 mm × 18 mm FR4 substrate (\(\varepsilon_r = 4.4, \tan\delta = 0.02, \ h = 1.2 \ mm\)) and were excited by the CPW transmission line using a 50-Ω SMA connector.

Fig. 2 displays the reflection coefficient and axial ratio (AR) for each design step. The blue box represents the target operating frequency range (6.24–8.24 GHz) corresponding to UWB channels 5, 6, 8, and 9, with Ant.1 being a linearly polarized slot antenna designed for comparison purposes. To achieve circular polarization, Ant.2 incorporated asymmetric slots and a CPW ground, as shown in Fig. 1(b). However, its AR remained above 3 dB within the 6.66–9.33 GHz range, thus failing to meet the target frequencies. To address this issue, in Ant.3, gamma-shaped slits were added to the slot. Ant.3 achieved an AR below 3 dB within the 6.31–8.14 GHz band. Furthermore, to optimize the reflection coefficient and AR, the monopole shape was modified into a gamma shape in Ant.4. Consequently, the simulated reflection coefficients of the proposed antenna were found to be below −10 dB within the 5.74–9.18 GHz range, while the simulated AR was below 3 dB in the 5.70–8.50 GHz range, thus aligning with the target operating frequencies. The disparities between the measurement and simulation outcomes may be ascribed to inaccuracies stemming from fabrication and measurement procedures.

Fig. 3 illustrates the current distribution in the proposed antenna at 7.3 GHz. It is evident that the proposed antenna exhibits right-handed circular polarization (RHCP) characteristics in the +z direction and left-handed circular polarization (LHCP) characteristics in the −z direction.

Furthermore, Fig. 4 depicts the radiation pattern of the proposed antenna in the xz- and yz-planes at two specific frequencies (6.9 GHz and 7.6 GHz) within the target UWB channel. The measured RHCP and LHCP radiation patterns are observed to be in close agreement with the simulation results of both planes. The simulated peak realized gains are recorded at 2.69 dBi and 3.77 dBi at 6.9 GHz and 7.6 GHz, respectively, while the measured peak realized gains are slightly higher, measuring 2.85 dBi and 4.02 dBi at 6.9 GHz and 7.6 GHz, respectively.

III. TIME-DOMAIN ANALYSIS

This section analyzes the performance of the proposed antenna in the time domain using the CST electromagnetic simulator. The fidelity factors were computed by comparing the in-
put pulse with the radiated E-fields. Furthermore, to investigate circular polarization attributes, this study conducted a cross-correlation analysis involving the input pulse and both the phi and theta components of radiated E-fields.

Fig. 5 illustrates the antenna fidelity factor (AFF) in both planes, considering both phi and theta polarizations. In the \( xz \)-plane, the AFF exceeds 0.9 for all angles in both polarizations. Meanwhile, in the \( yz \)-plane, the AFF is greater than 0.8 for all angles in the phi polarization, whereas it exceeds 0.8 for all angles in the theta polarization except for 270°, where the factor is valued at 0.70. This relatively low AFF at 270° may be attributed to significant fluctuations in gain across the operating frequency range.

Fig. 6 presents the normalized transmitted and received pulse signals, which were utilized to evaluate the system fidelity factor (SFF). For this purpose, two identical proposed antennas with a separation of 500 mm in both face-to-face and side-by-side configurations were arranged. The SFFs for the side-by-side and face-to-face setups were 92.5% and 98.4%, respectively.

IV. CONCLUSION

This letter introduces a novel CPW-fed CP slot antenna specifically designed for UWB applications. This antenna features innovative design elements, including an asymmetric ground equipped with gamma-shaped slits to achieve circular polarization and a gamma-shaped monopole to enhance reflection coefficients. Meticulous design optimization enables the proposed antenna to demonstrate consistent performance within the desired operating frequency range, which also aligns with UWB channels. The time-domain analysis shows good antenna fidelity, while the radiation patterns closely match the simulation results. Therefore, the proposed antenna exhibits great promise for UWB applications, in turn contributing to advancements in wireless communication and positioning technology.

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REFERENCES